

Attachment 3.10

**X-TRACK CALIBRATION
ON ORBIT CONTAMINATION
SCAN MIRROR MONITORING
QMR SPLINTER MEETING**

11 MARCH 1992



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CONTAMINATION EFFECTS ON CROSSTRACK CALIBRATION

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- **ASSUMPTIONS:**
 - **CONTAMINATION LEVEL (5 YEAR) GSFC MODEL 55-77A THICKNESS**
 - **CONTAMINANT SPECIES: CARBON AND SILICON OXIDE**
 - **DEPOSITED AS CONTINUOUS THIN FILM**
- **SBRC MODELING DOCUMENTED IN "MODIS-N CROSSTRACK RADIOMETRIC CALIBRATION VARIATION AS A FUNCTION OF SCAN MIRROR CONTAMINATION" PL3095-N-00360**
- **CARBON CONTAMINANT HAS MUCH GREATER EFFECT THAN SILICON OXIDE**
- **"IF" GSFC AND SBRC MODELING IS CORRECT CONTAMINATION IS A MAJOR PROBLEM.
NO EVIDENCE OF LANDSAT DEGRADATION DUE TO CONTAMINATION**

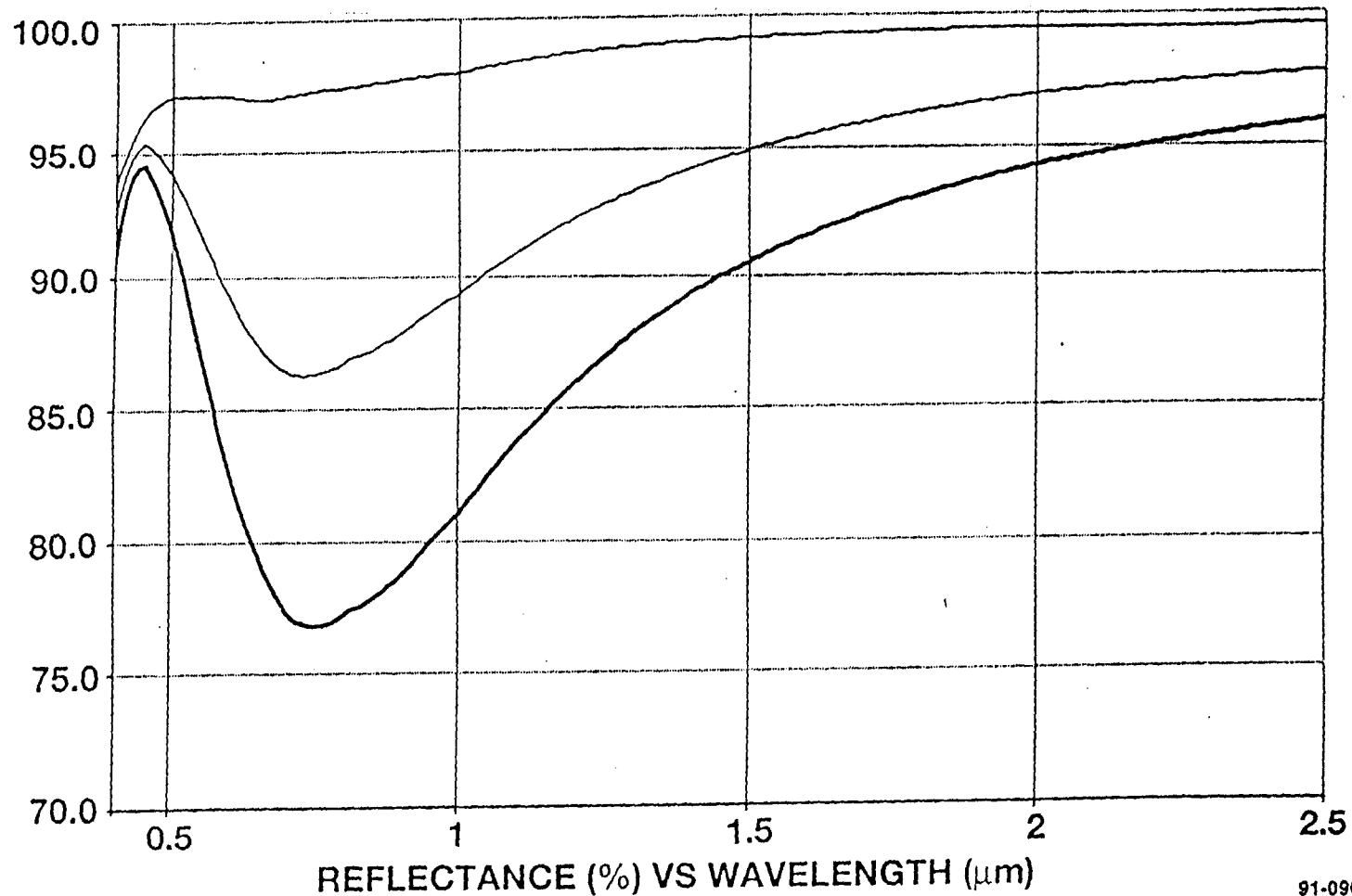
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91-0908-816



SCAN MIRROR SPECTRAL REFLECTANCE; AOI 37°; CARBON 0, 25A, 50A



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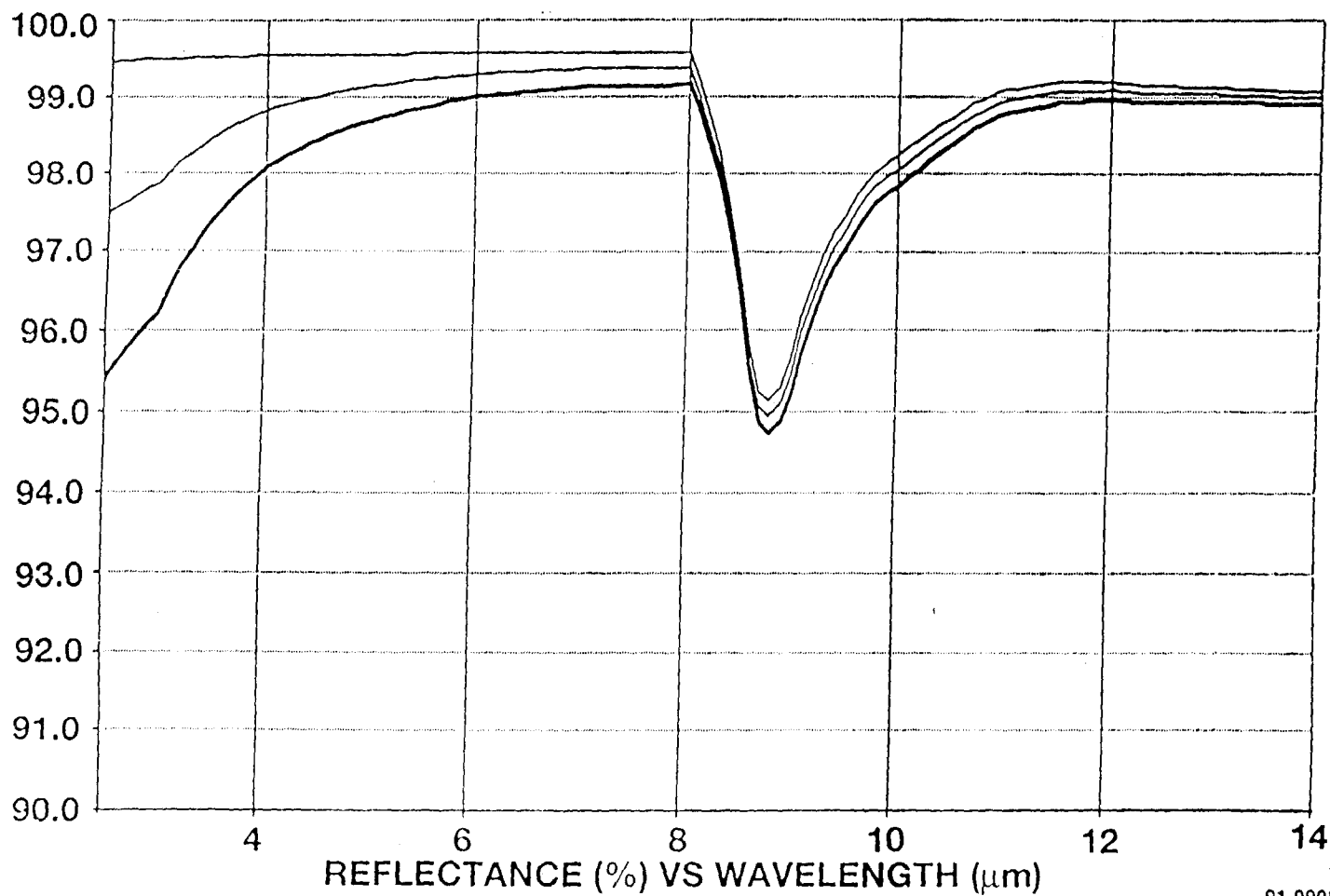
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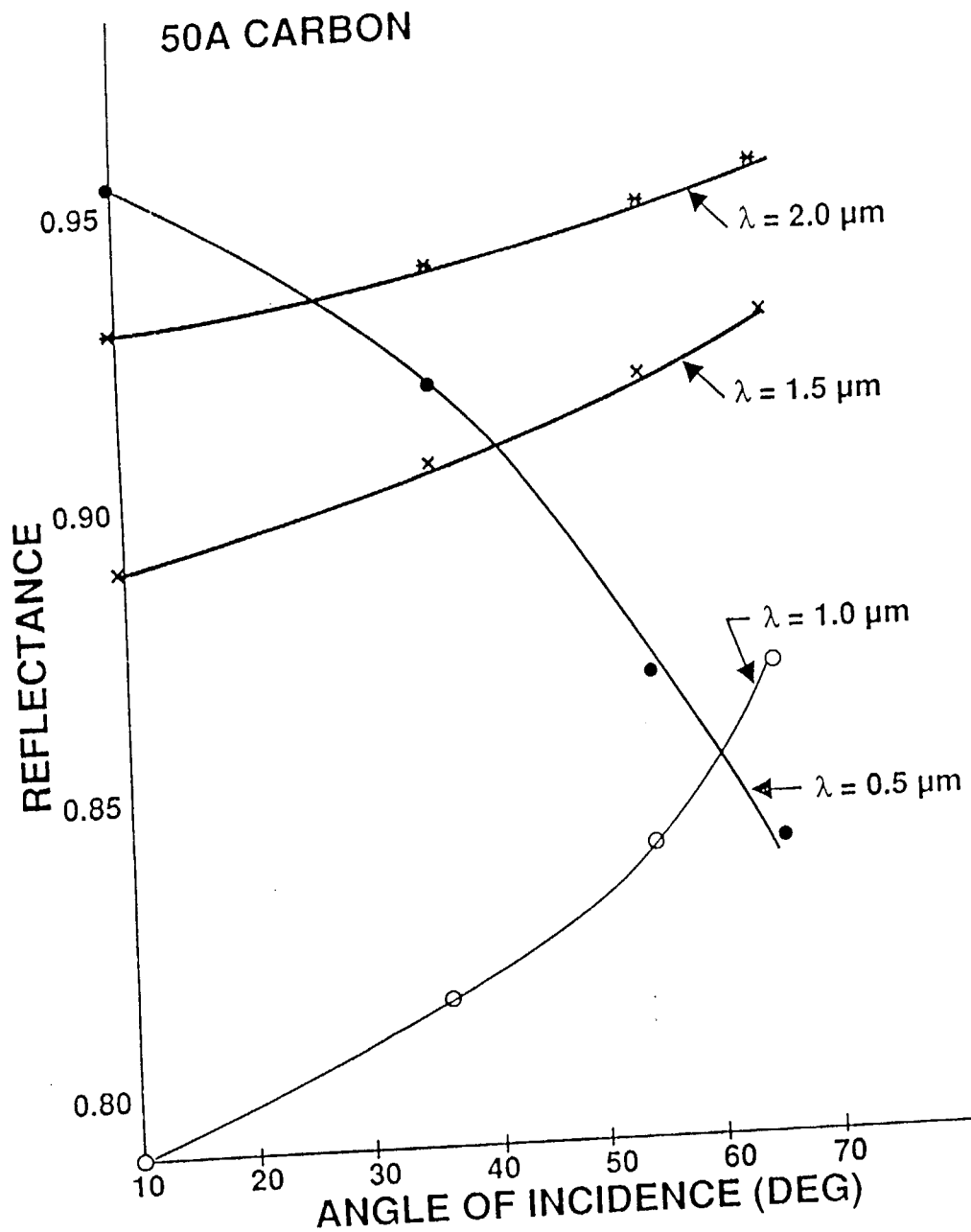
SCAN MIRROR SPECTRAL REFLECTANCE; AOI 37°; CARBON 0, 25A, 50A



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**EFFECT OF
50A CARBON
CONTAMINATION
ON SCAN MIRROR
REFLECTANCE
IN VIS/NIR/SWIR
REGIONS**



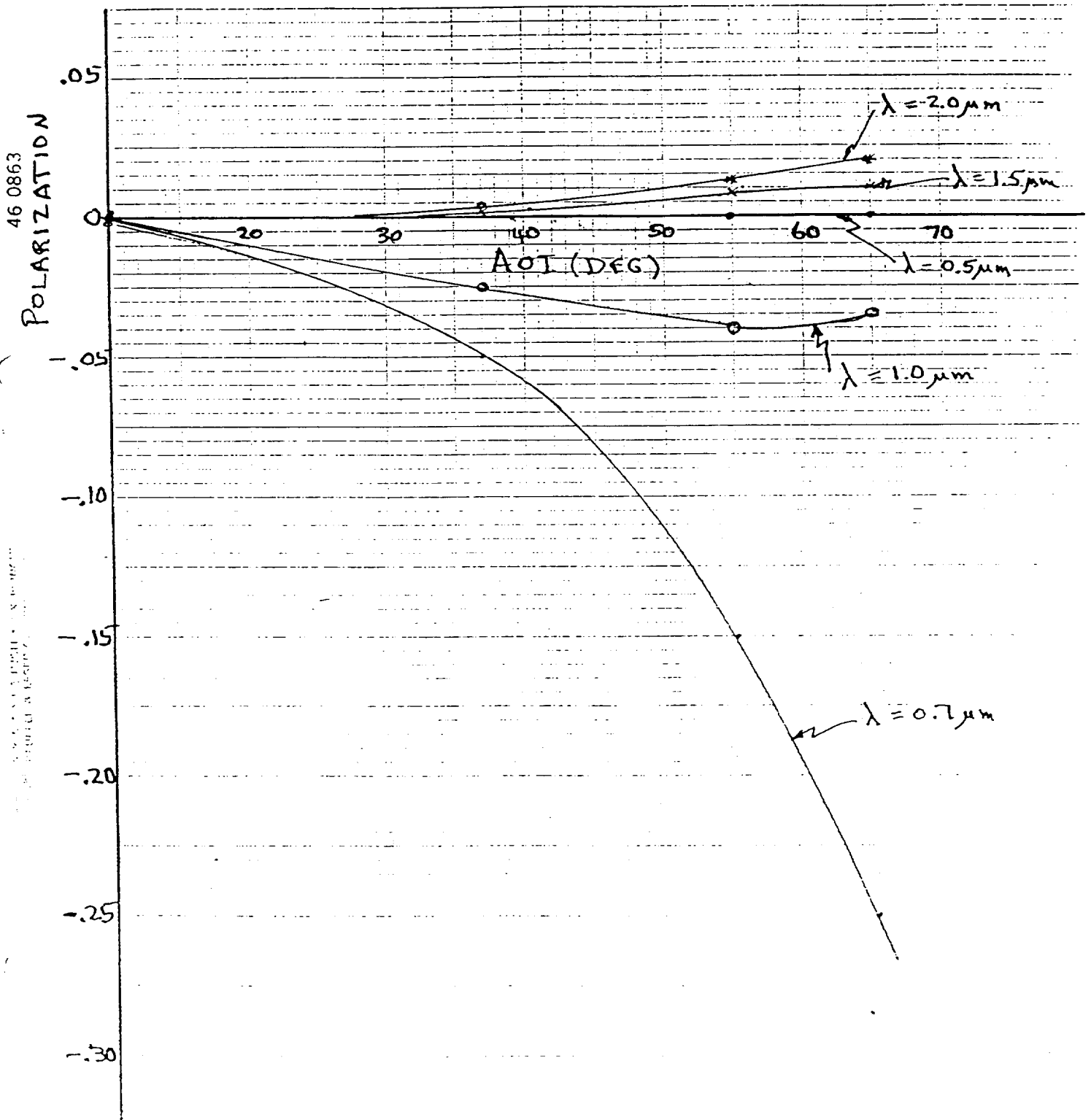
11/91
91-0908-821

To: J.L. Engel
From: J.B. Young
G.F. Moore
Subj: MODIS-N Cross Track Radiometric
Calibration Variation as a Function of Scan
Mirror Contamination

11/20/91
Ref: 91.8222.2342
Ref: PL3095-N-00360

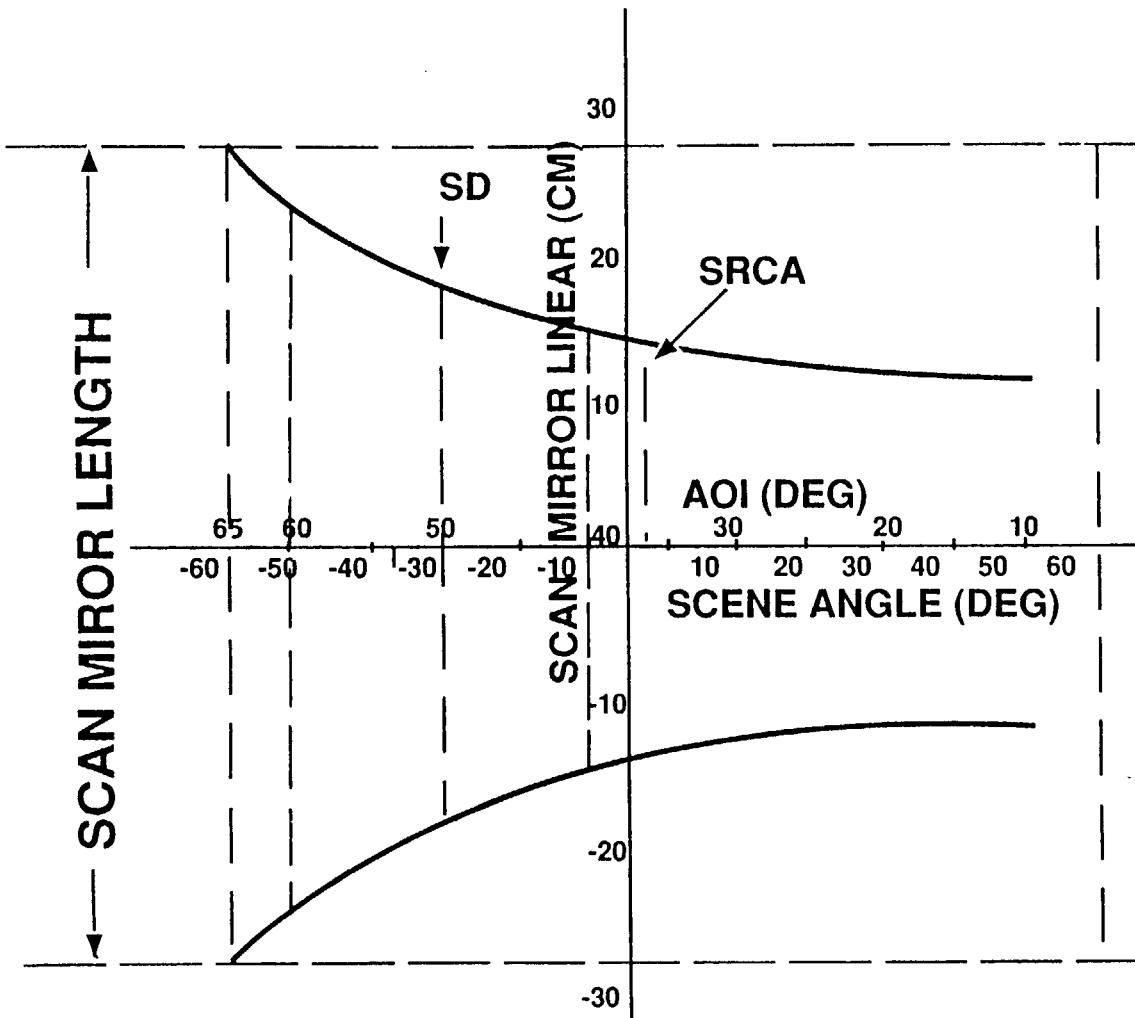
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Figure 27 Polarization as a function of AOI for selected wavelengths in
VIS/NIR/SWIR
Contaminant: Carbon 50A





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WITH ON ORBIT
CONTAMINATION
CROSS TRACK
CALIBRATION
DEPENDENT
UPON
 ρ VS. AOI



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ON ORBIT MONITORING METHODS

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- **MODIFY SRCA (INCLUDING ADDITIONAL DETECTORS)**
- **LAMPS (W/O OPTICS) LOCATED IN SCAN MIRROR CAVITY**
 - **USE MODIS-N SYSTEM DETECTORS**
 - **SNR MODEL GENERATED**
- **POSSIBLE USE OF SOLAR SOURCE**
 - **SDSM TYPE DETECTION**
 - **METHOD OF USING SUN - NOT KNOWN**
- **GROUND TRUTH USING UNDER FLIGHTS**
 - **SIMILAR TO AVHRR**



EVALUATION OF CONTAMINATION METHODOLOGY



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EVALUATION MATRICES					
PERCEIVED REQUIRED CALIBRATION DATA IMPORTANCE					
SCAN MIRROR	VIS	NIR	SWIR	MWIR	LWIR
SPATIAL	LOW	LOW	LOW	LOW	LOW
SPECTRAL	HIGH	HIGH	MODERATE	LOW	LOW
ANG OF INC	HIGH	HIGH	MODERATE	LOW	LOW
POLARIZATION	MODERATE	MODERATE	LOW	LOW	LOW
DIFFICULTIES ASSOCIATED WITH STRAWMAN MEASUREMENT METHOD					
SCAN MIRROR	VIS	NIR	SWIR	MWIR	LWIR
SPATIAL	HIGH	HIGH	HIGH	HIGH	HIGH
SPECTRAL	MODERATE	MODERATE	HIGH	HIGH	HIGH
ANG OF INC	MODERATE	MODERATE	HIGH	HIGH	HIGH
POLARIZATION	HIGH	HIGH	HIGH	HIGH	HIGH

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9



RADIOMETRIC/POLARIMETRIC PERFORMANCE STRONGLY DEPENDENT UPON:



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- CONTAMINANT TYPE - N,K
- CONTAMINANT THICKNESS
- FORMATION - CONTINUOUS FILM VS "CLUMPS"
- CROSSTACK ANGLE - AOI
- SPECTRAL LOCATION

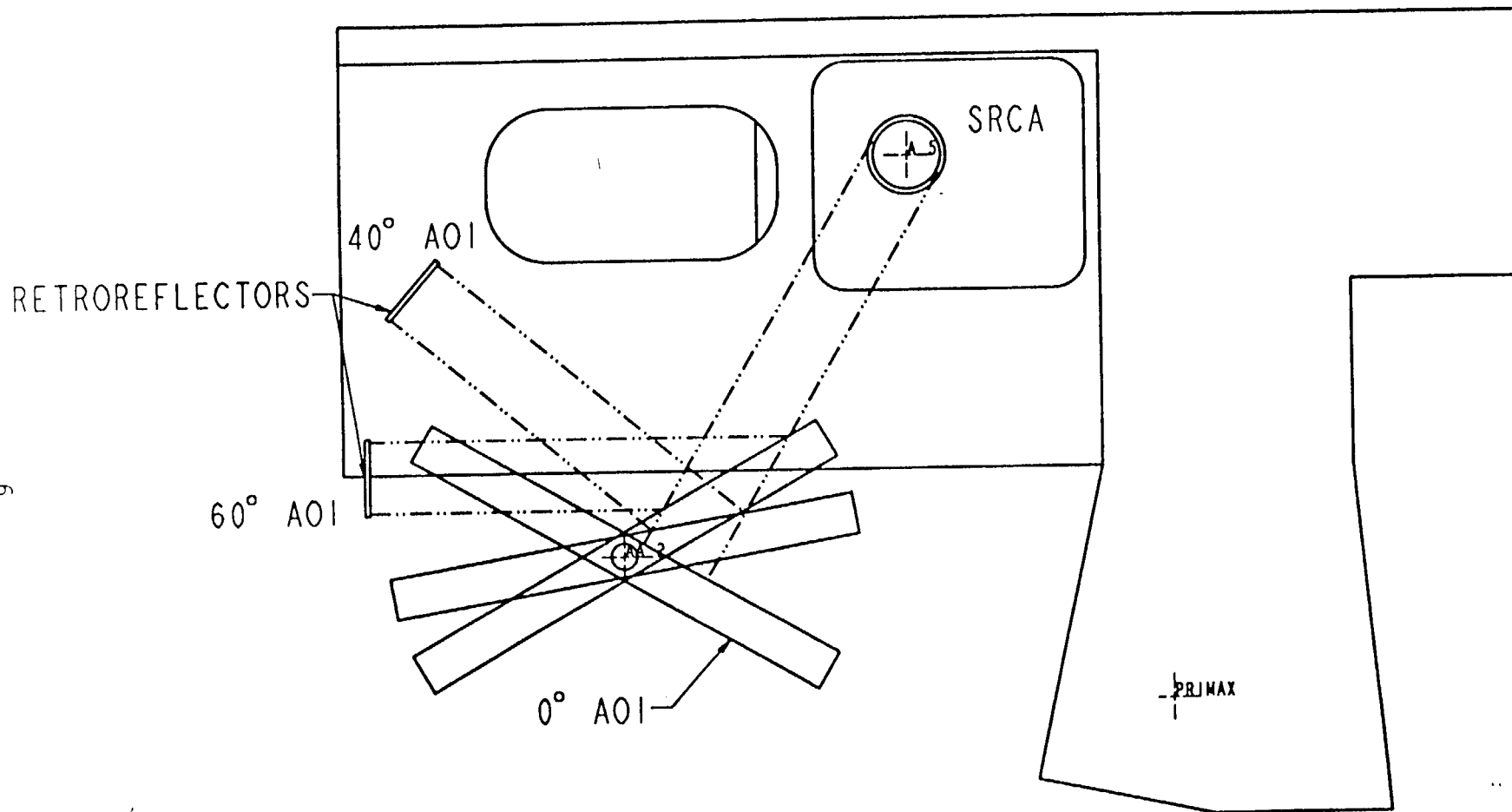


Figure 3 Use of modified SRCA to achieve scan mirror reflectance measurement at AOI: 0°, 40°, 60°.

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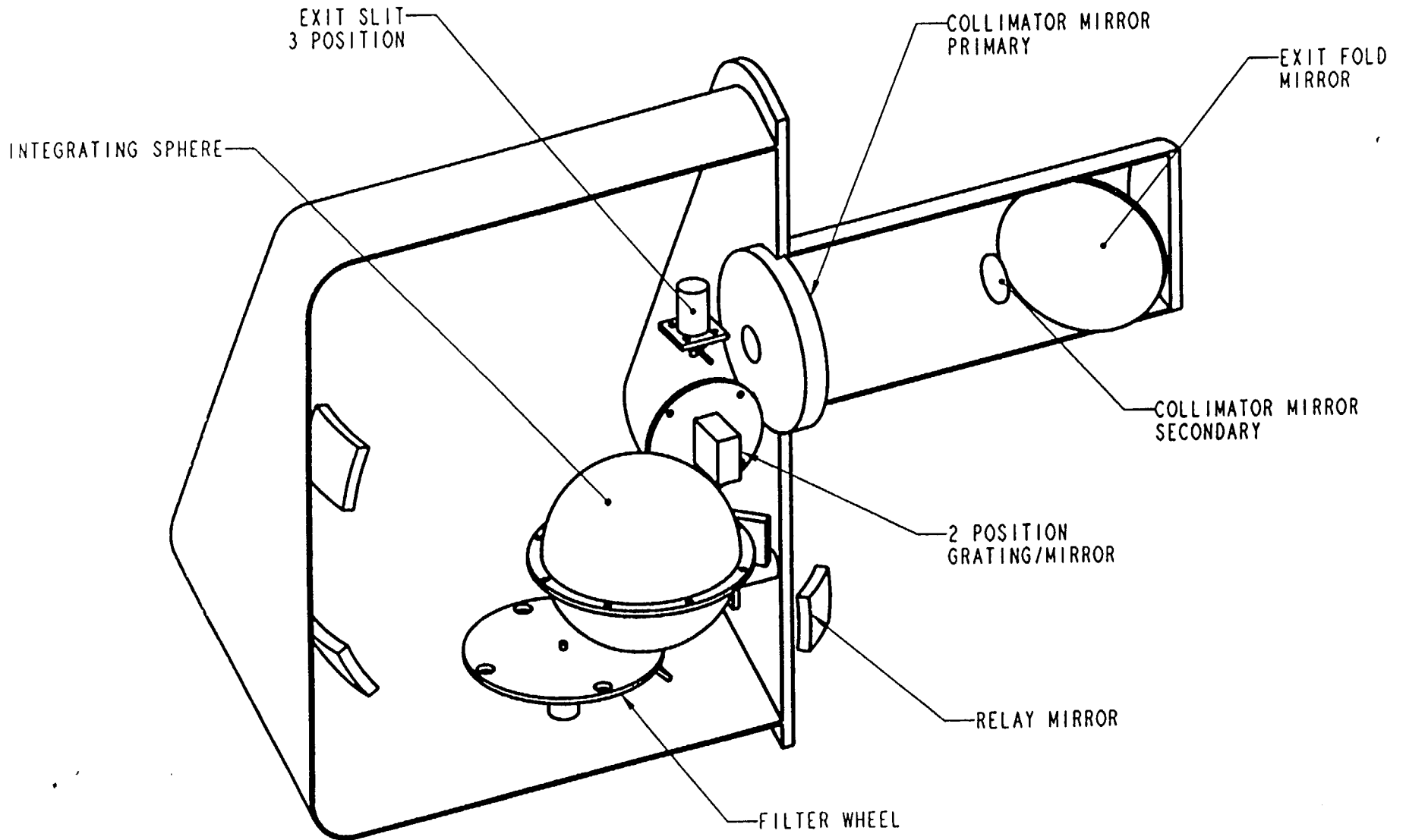


SRCA HARDWARE MODIFICATIONS

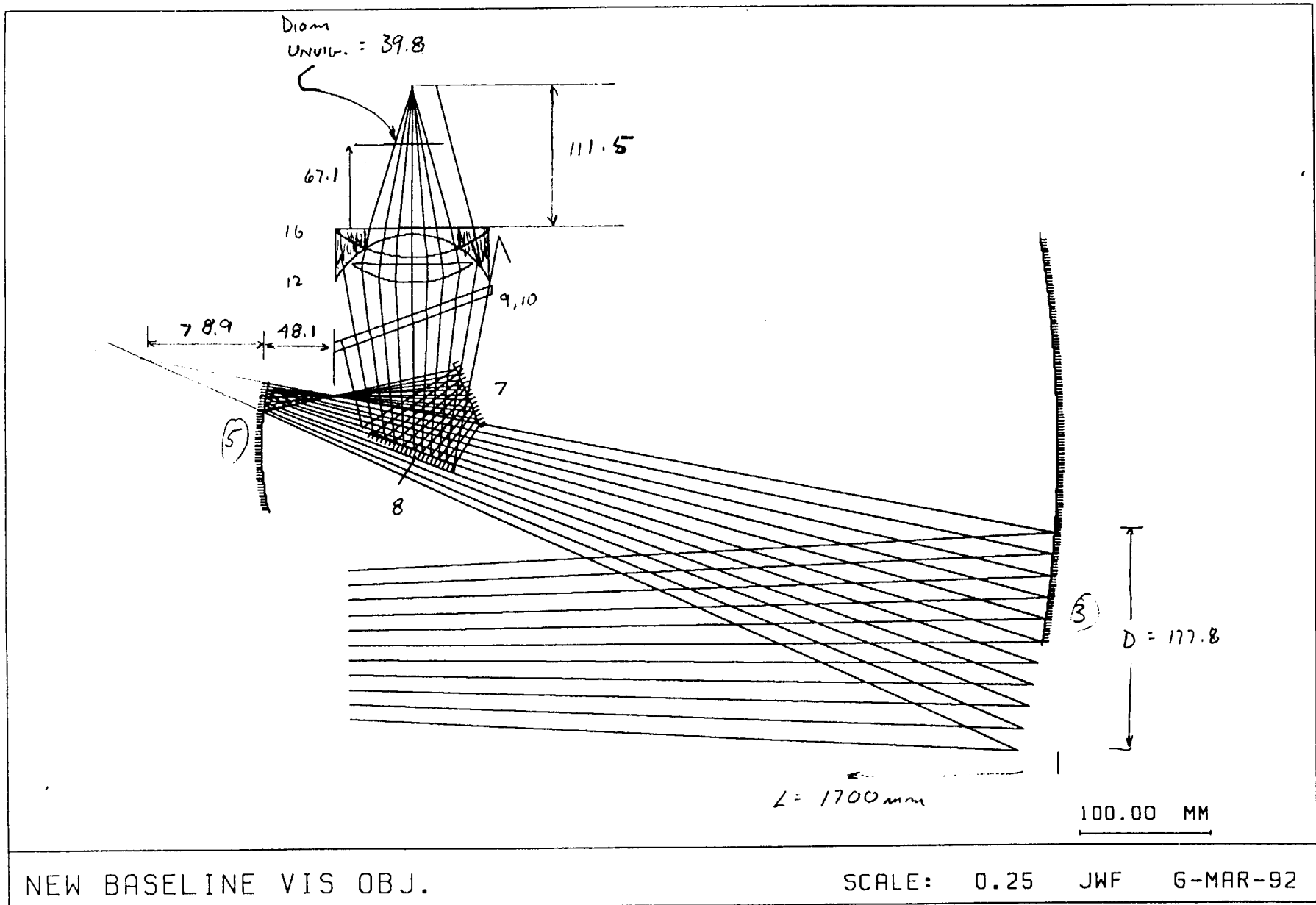


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- TWO RETROREFLECTORS
- Si DETECTOR AT EXIT SLITS
- SET OF ORTHOGONAL POLARIZERS/ORDER FILTERS
- TILTABLE FOLD MIRROR - SELF CALBIRATION



PIZ



Save, (Y)es or (N)o <Yes> ?

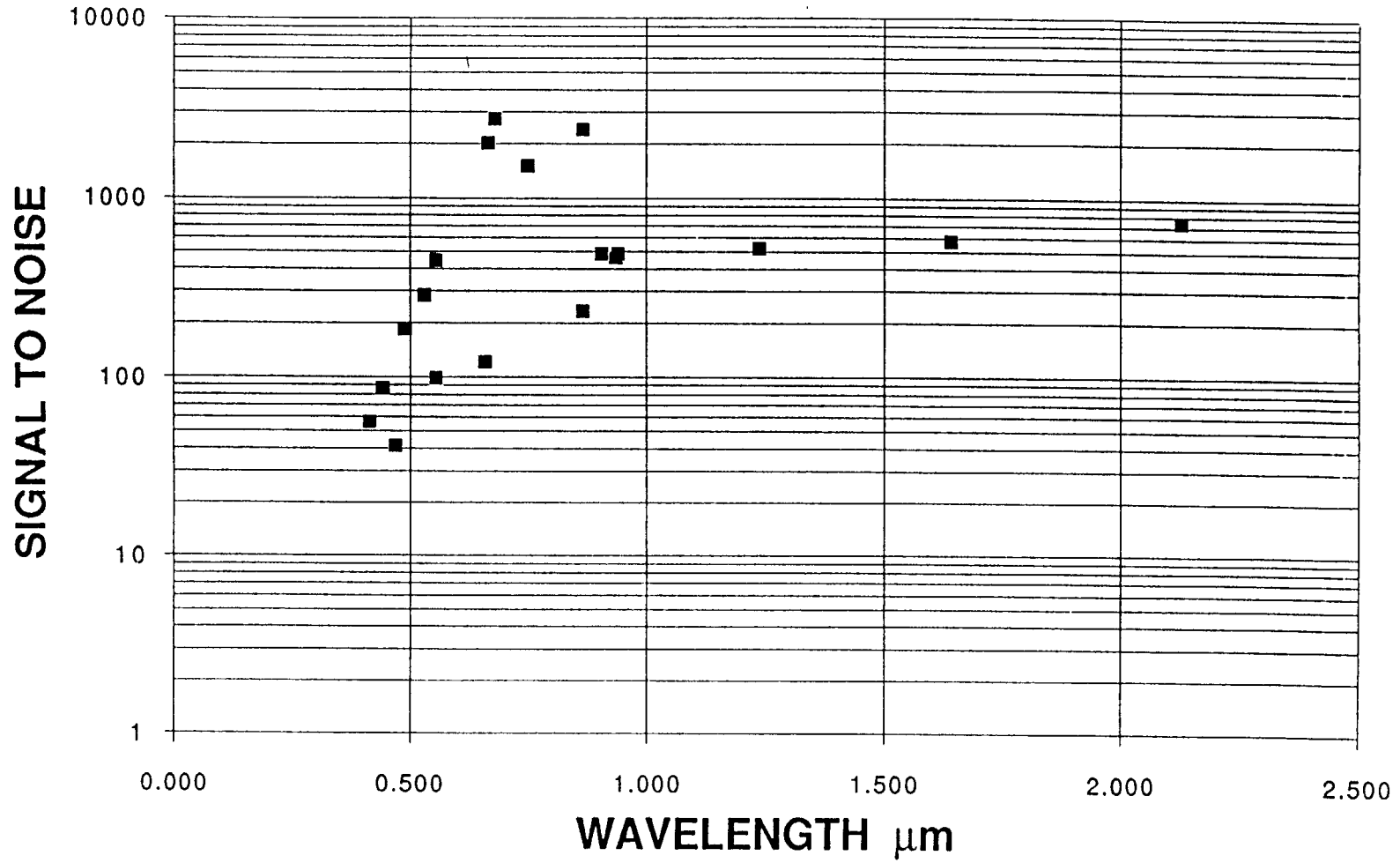
Contam 2

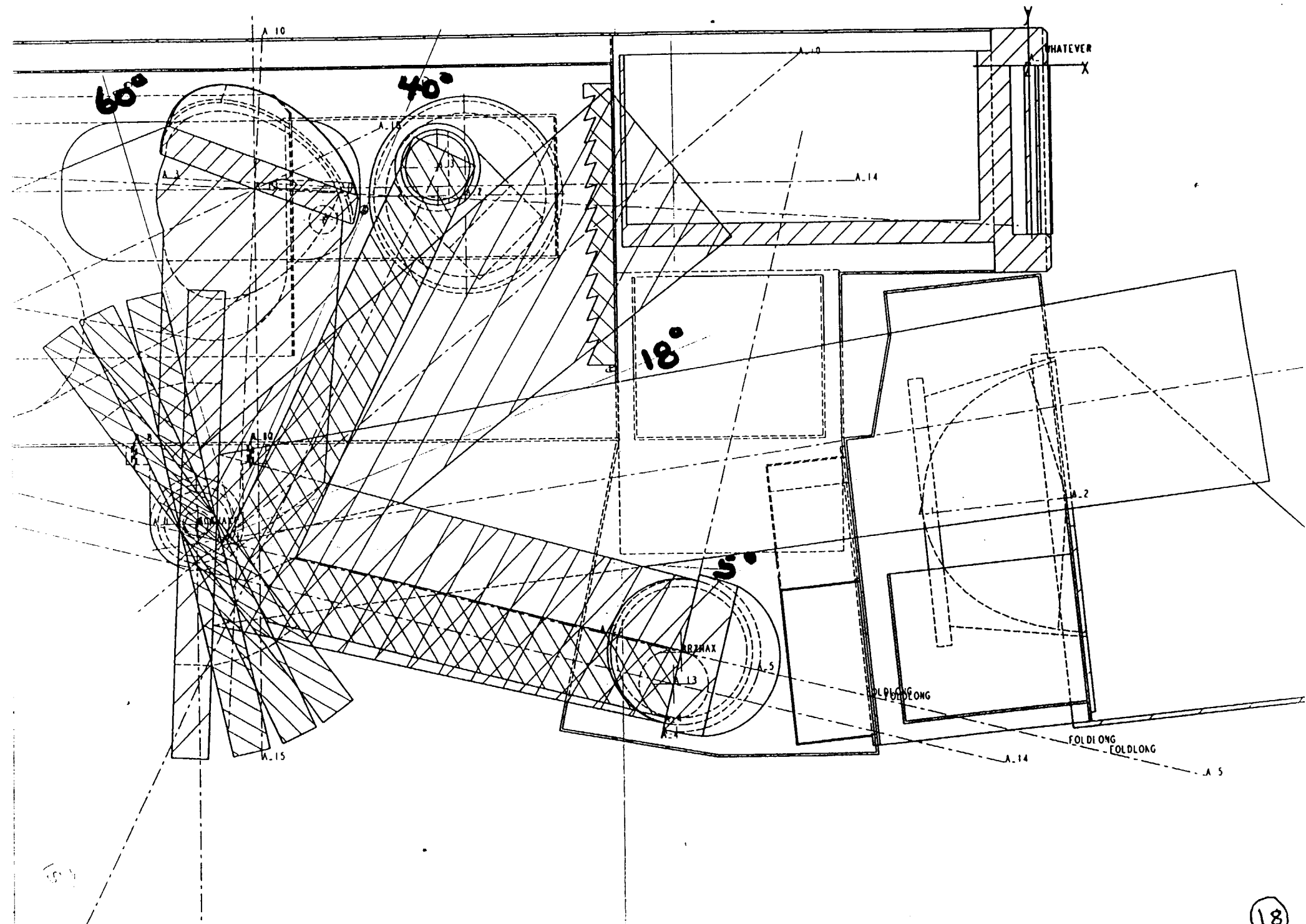
THIS IS A REVIEW OF THE POSSIBILITY OF USING A LAMP IN THE SCAN MIRROR CAVITY TO MONITOR CONTAMINATION							
THE EQUATIONS TO BE USED INCLUDE:							
$Ffs = K \cdot Emiss \cdot w \cdot L \cdot \Omega_{ent} \cdot F_{det} / (4 \cdot \pi \cdot L_{max} \cdot (\Omega \cdot A)_{modis})$							
$Emiss \cdot w = (0.7641 - 0.0000875 \cdot Temp) \cdot EXP(-(.759 - 0.0001488 \cdot Temp) \cdot Wln)$							
$L = 11905.7 / (Wln^5 \cdot (EXP(14388 / Temp / Wln) - 1))$							
$K = Pe \cdot Conv \text{ eff} / (\sum Emiss \cdot w \cdot L \cdot \Delta Wln)$ where $\sum Emiss \cdot w \cdot L \cdot \Delta Wln = SUM_Lw_wln$							
Note: \sum is taken over .4 to 5.0 micrometers							
WLN	Emiss	L	Lw	WLN	Emiss	L	Lw
0.4	0.445	5.88856	2.62145	3.6	0.160	6.84628	1.09449
0.5	0.431	22.10912	9.53245	3.7	0.155	6.27378	0.97138
0.6	0.418	45.16769	18.86088	3.8	0.150	5.75868	0.86354
0.7	0.404	66.78879	27.01086	3.9	0.145	5.29439	0.76891
0.8	0.392	81.95196	32.09927	4	0.141	4.87513	0.68572
0.9	0.379	89.73013	34.03885	4.1	0.136	4.49588	0.61246
1	0.367	91.38956	33.57639	4.2	0.132	4.15223	0.54783
1.1	0.356	88.78897	31.59347	4.3	0.128	3.84032	0.49072
1.2	0.345	83.60308	28.81120	4.4	0.124	3.55674	0.44017
1.3	0.334	77.08799	25.72922	4.5	0.120	3.29853	0.39535
1.4	0.323	70.09183	22.65730	4.6	0.116	3.06304	0.35557
1.5	0.313	63.14326	19.76827	4.7	0.112	2.84795	0.32018
1.6	0.303	56.54579	17.14521	4.8	0.109	2.65120	0.28868
1.7	0.294	50.45433	14.81637	4.9	0.105	2.47098	0.26058
1.8	0.284	44.93049	12.77866	5	0.102	2.30566	0.23549
1.9	0.275	39.98010	11.01258				
2	0.267	35.57765	9.49124			SUM_Lw_wln	41.57503
2.1	0.258	31.68165	8.18568				
2.2	0.250	28.24400	7.06763				
2.3	0.242	25.21552	6.11106				
2.4	0.235	22.54901	5.29269				
2.5	0.227	20.20081	4.59218				
2.6	0.220	18.13148	3.99194				
2.7	0.213	16.30593	3.47694				
2.8	0.207	14.69325	3.03438				
2.9	0.200	13.26637	2.65342				
3	0.194	12.00174	2.32487				
3.1	0.188	10.87889	2.04098				
3.2	0.182	9.88005	1.79521				
3.3	0.176	8.98985	1.58201				
3.4	0.170	8.19494	1.39670				
3.5	0.165	7.48376	1.23532				
3.6	0.160	6.84628	1.09449				

Contam 2

POWER Pe=	18.600								
Conv eff=	0.600								
Temp(K)=	2950.0	Ffs=	$K \cdot \text{Emiss}_w \cdot L \cdot \text{PI}() \cdot \text{Dent}^{2/4} / \text{Zlamp_ent}^{2/4} \cdot \text{Fdet} / (4 \cdot \text{PI}() \cdot \text{Lmax} \cdot (\text{IFOV} / 705000)^2 \cdot \text{PI}() \cdot \text{Dent}^{2/4})$						
K=	0.2684	SNR_lamp=	Ffs * SNR_syst						
Fdet=	$(\text{IFOV} / 705000 \cdot \text{Fsyst})^2 / (\text{PI}() \cdot (\text{Zlamp_fpa} / \text{Frat_lamp})^{2/4})$								
Band	LMAX	SNR	IFOV	Wln	Emiss_w	L	Fdet	Ffs	SNR_lamp
		syst							
1.	0.0685	4053.	250	0.659	0.410	58.528	0.000015	0.030	122
2.	0.0285	2317.	250	0.865	0.384	87.793	0.000015	0.102	236
3.	0.0593	4090.	500	0.470	0.435	16.163	0.000059	0.010	42
4.	0.0518	4079.	500	0.555	0.424	34.500	0.000059	0.024	99
5.	0.0068	1511.	500	1.240	0.340	81.101	0.000059	0.349	528
6.	0.0070	2917.	500	1.640	0.299	54.043	0.000059	0.199	580
7.	0.0022	2444.	500	2.130	0.256	30.604	0.000059	0.306	749
8.	0.0175	3431.	1000	0.415	0.443	7.612	0.000234	0.017	57
9.	0.0133	2660.	1000	0.443	0.439	11.543	0.000234	0.033	87
10.	0.0101	2525.	1000	0.490	0.433	20.044	0.000234	0.074	186
11.	0.0082	2216.	1000	0.531	0.427	28.926	0.000234	0.130	287
12.	0.0064	2286.	1000	0.555	0.424	34.500	0.000234	0.196	449
13.	0.0032	3077.	1000	0.667	0.409	60.219	0.000234	0.662	2036
14.	0.0031	3875.	1000	0.681	0.407	63.090	0.000234	0.712	2761
15.	0.0026	1529.	1000	0.750	0.398	75.311	0.000234	0.992	1517
16.	0.0016	1333.	1000	0.865	0.384	87.793	0.000234	1.811	2414
17.	0.0185	3083.	1000	0.905	0.379	89.943	0.000234	0.158	488
18.	0.0256	4063.	1000	0.936	0.375	90.937	0.000234	0.115	466
19.	0.0189	3150.	1000	0.940	0.375	91.026	0.000234	0.155	489
Fsyst=	38.000	LAMP IMAGING							
Dent=	17.780	Zpm_lamp	69.635	$.= (1 / \text{Fpm} - 1 / \text{Zlamp_ent})^{(-1)}$					
Frat_syst=	2.137	Zsm_lamp=	4.813	$.= (1 / \text{Fsm} - 1 / (\text{Zpm_sm} - \text{Zpm_lamp}))^{(-1)}$					
Zlamp_ent	170.000	Zobj_lamp=	13.478	$.= (1 / \text{Fobj} - 1 / (\text{Zsm_obj} - \text{Zsm_lamp}))^{(-1)}$					
Fpm=	49.400	Zlamp_fpa=	3.978	$.= \text{Zobj_lamp} - \text{Fobj}$					
Zpm_sm=	61.750								
Fsm=	12.350	Frat_lamp=	1.001	$.= (\text{Zep_obj} - \text{Zobj_lamp}) / \text{Dep_obj}$					
Zsm_obj=	37.000								
Fobj=	9.500								
Zep_sm=	15.438	$.= (1 / \text{Fsm} - 1 / (\text{Fpm} + \text{Fsm}))^{(-1)}$							
Dep_sm=	4.445	$.= \text{Dent} \cdot \text{Zep_sm} / \text{Zpm_sm}$							
Zep_obj=	16.982	$.= (1 / \text{Fobj} - 1 / (\text{Zsm_obj} - \text{Zep_sm}))^{(-1)}$							
Dep_obj=	3.501	$.= \text{Dep_sm} \cdot \text{Zep_obj} / (\text{Zsm_obj} - \text{Zep_sm})$							

CONTAMINATION MEASUREMENT - SNR







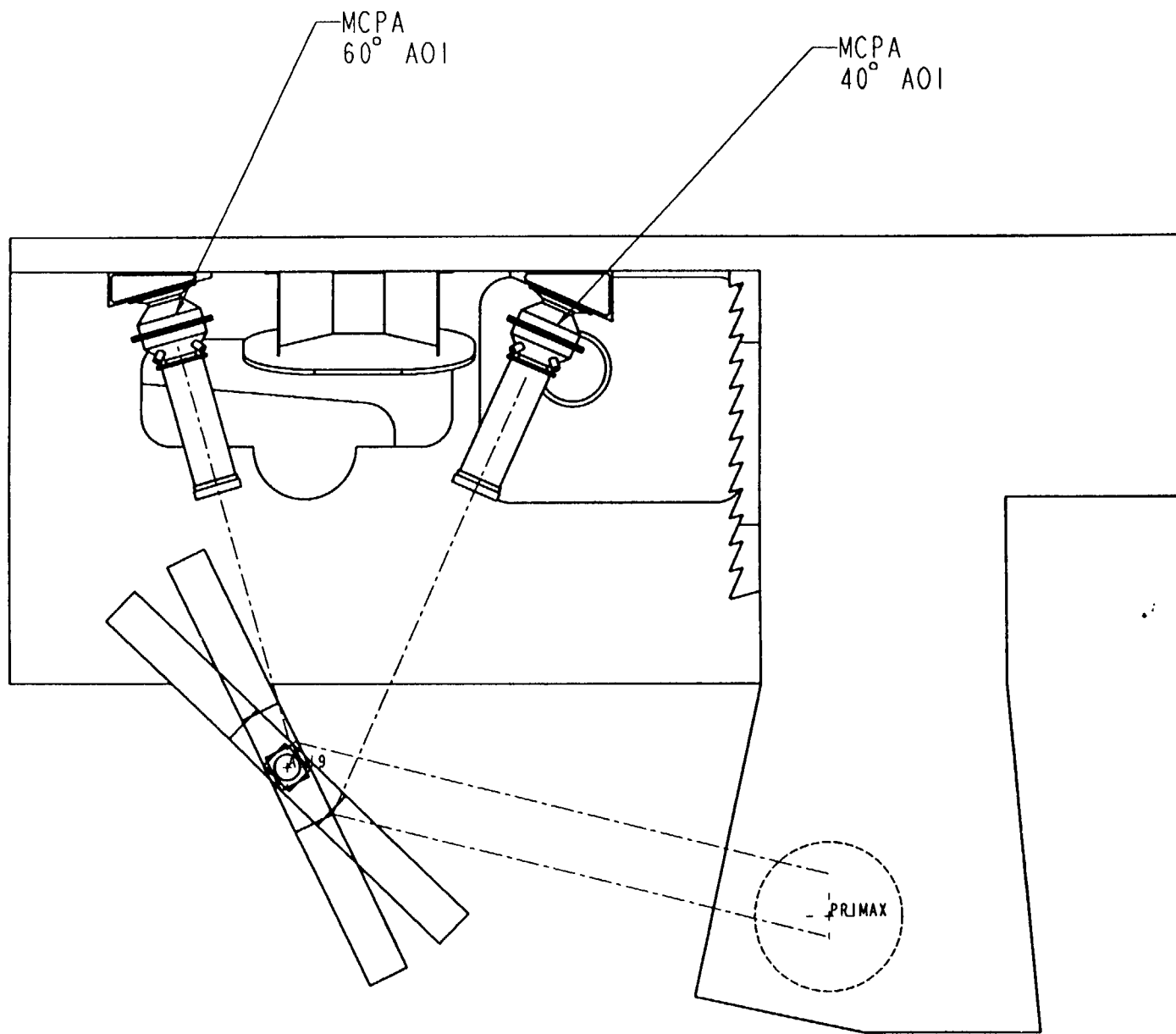
ALL METHODS HAVE LIMITATIONS

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- **ELEMENTS OTHER THAN SCAN MIRROR CAN BE CONTAMINATED**
- **LAMP METHOD CAN COVER MORE SPECTRAL RANGE BUT DOES NOT HAVE POLARIZATION CAPABILITY**
- **MODIS DETECTOR VIEWS LAMP ENERGY THROUGH A RANGE OF SCAN MIRROR AOI AND SPATIAL AREAS**

MAY BE ASSET AND/OR LIABILITY



PROPOSED CONFIGURATION FOR MIRROR POLARIZATION CALIBRATOR ASSEMBLY (MCPA)

